Measurements of phonatory power flows and efficiencies in a human airway phantom

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OVERVIEW

We present empirical characterization of phonation power flows and efficiencies for three distinct regions of a human airway phantom: the larynx, the vocal tract, and the combination of larynx and vocal tract. A control volume power flow formulation [1], which identified inputs, outputs and losses in terms of joint statistics between volume flow and pressure, guided the measurements. The measurements presented here are used to estimate the terms in the energy equation for the larynx, the vocal tract and the system composed of their combination. From these estimates the efficiencies are also estimated.

References

[1] Krane, M., et al., Proc. of 11th ICVPB, E. Lansing, MI, 2018. [2] Schutte, H. The efficiency of voice production. PhD diss. 1980. [3] Isshiki, N. Vocal fold physiology, 193-203, 1981. [4] Titze, et al., J. Voice, 30(4) 398-406, 2015. [5] Campo, L. MS Thesis, Penn State Univ., 2012. [6] McPhail, et al JASA 146(2) 1230-1238, 2019. [7] Chung, J. & Blaser, D., JASA 68(3), 1980a. [8] Chung, J. & Blaser, D., JASA 68(3), 1980b.

GOALS

- Develop physical basis for voice efficiency measures
- Characterize aeroelasticaeroacoustic power flows characteristic of phonation
- Measure power flows and
- efficiencies in airway phantom

COVER

0.4

0.6



[9] Chung, J. & Blaser, D., JASA 68(6), 1980c.

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We estimated the work terms used in computing efficiency.



Signal processing

We used the measured acoustic pressures $\hat{p}_1, \hat{p}_2, \hat{p}_3, \hat{p}_4$ to estimate the following work terms, which are in the form of variances and covariances:



$Q_{A}'^{2} \qquad Q_{D}'^{2} \qquad p_{A}'' Q_{A}' \qquad p_{D}'' Q_{D}' \qquad p_{m}' Q_{m}'$

The reflection coefficients at microphones 2 and 3 are estimated from the G_{ii} cross-spectra of the pressures measured by microphones :

$$R_{3} = \frac{\frac{G_{34}}{G_{33}} - e^{-ik(x_{4} - x_{3})}}{e^{+ik(x_{4} - x_{3})} - \frac{G_{34}}{G_{33}}}, \quad R_{2} = \frac{\frac{G_{21}}{G_{22}} - e^{-ik(x_{4} - x_{3})}}{e^{+ik(x_{4} - x_{3})} - \frac{G_{21}}{G_{22}}},$$

The reflection coefficients at the locations of interest are then given by:

$$R_A = R_3 e^{-i2k(x_3 - x_A)}, \quad R_D = R_2 e^{+i2k(x_D - x_2)}, \quad R_m = R_2 e^{+i2k(x_m - x_2)}$$

We compute variances, covariances in terms of the autospectra of the measured pressures and the reflection coefficients at the location of interest (Chung and Blaser, 1980a, b, c):

$$\overline{p_{A}^{+\prime}Q_{A}^{\prime}} = 2\frac{S}{\rho_{0}c}\int_{0}^{+\infty} \operatorname{Re}\left(\frac{G_{33}}{1+R_{A}}\right)df, \quad \overline{Q_{A}^{\prime 2}} = 2\left(\frac{S}{\rho_{0}c}\right)^{2}\int_{0}^{+\infty} \frac{G_{33}}{G_{33}}\operatorname{Re}\left(\frac{1-2\operatorname{Im}\left\{R_{A}\right\}-\left|R_{A}\right|^{2}}{\left|1+R_{A}\right|^{2}}\right)df$$

$$\overline{p_{D}^{-\prime}Q_{D}^{\prime}} = 2\frac{S}{\rho_{0}c}\int_{0}^{+\infty} \operatorname{Re}\left(\frac{G_{22}}{1+R_{D}}\right)df, \quad \overline{Q_{D}^{\prime 2}} = 2\left(\frac{S}{\rho_{0}c}\right)^{2}\int_{0}^{+\infty} \frac{G_{22}}{G_{22}}\operatorname{Re}\left(\frac{1-2\operatorname{Im}\left\{R_{D}\right\}-\left|R_{D}\right|^{2}}{\left|1+R_{D}\right|^{2}}\right)df$$

$$\overline{p_{m}^{\prime}Q_{m}^{\prime}} = 2\frac{S}{\rho_{0}c}\int_{0}^{+\infty} \operatorname{Re}\left(\frac{G_{22}}{1+2\operatorname{Im}\left\{R_{m}\right\}-\left|R_{m}\right|^{2}}{\left|1+R_{m}\right|^{2}}\right)df$$

RESULTS: Efficiencies





SUMARY



- Defined efficiencies in terms of cycle-averaged terms, guided by control volume analysis
- Inferred necessary pressure, volume flow variances and pressure-volume flow covariances using extension of 2-microphone technique
- Pressure-volume flow covariances comprise the energy transfers relevant for efficiency
- Estimated laryngeal, vocal tract, and system efficiencies for vocal fold vibration in airway phantom

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